

4.2 Geometric Design Principles of At-Grade Intersections

Design Principles of At-Grade Intersections

- The fundamental objective is to minimize the severity of potential conflicts among different streams of traffic and between pedestrians and turning vehicles.
- At the same time, it is necessary to provide for the smooth flow of traffic across the intersection.

The design should incorporate the operating characteristics of both vehicles and pedestrians.

Design Principles of At-Grade Intersections

- The corner radius of an intersection pavement should not be less than either the turning radius of the design vehicle or the radius required for design velocity of the turning roadway under consideration.
- It should also ensure adequate pavement widths of turning roadways and approach sight distances.

At-grade intersections should not be located at or just beyond sharp crest vertical curves or at sharp horizontal curves.

Design Principles of At-Grade Intersections

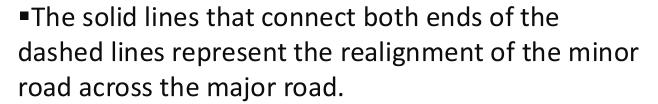
- 1 Alignment of At-Grade Intersections
- **2** Profile of At-Grade Intersections
- **3** Curves at At-Grade Intersections
- (4) Channelization of At-Grade Intersections
- (5) Minimum Pavement Widths of Turning Roadways
- **6** Sight Distance at Intersections

1 Alignment of At-Grade Intersections

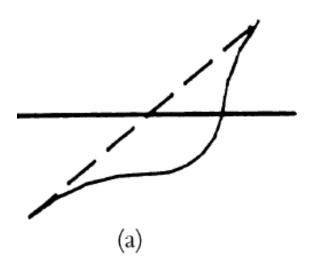
- The best alignment is when the intersecting roads meet at right or nearly right angles, and it is superior to acute-angle alignments.
- At right or nearly right angles intersections:
 - Much less road area is required for turning
 - There is a lower exposure time for vehicles crossing the main traffic flow
 - Visibility limitations (particularly for trucks) are not as serious as those at acute-angle intersections

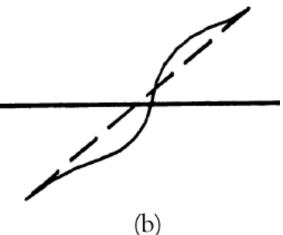
1 Alignment of At-Grade Intersections

- Figure (a) and (b) show alternative methods for realigning roads intersecting at acute angles to obtain a nearly right-angle intersection.
- ■The dashed lines in this figure represent the original minor road as it intersected the major road at an acute angle.



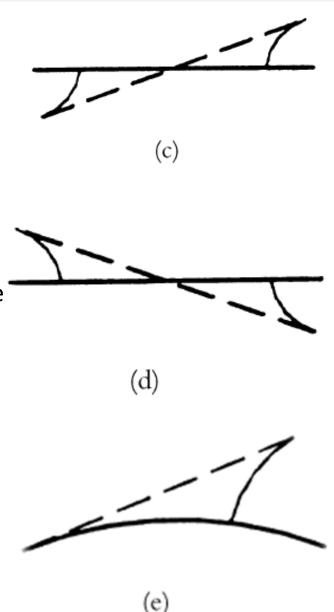
■care must be taken to ensure that the realignment provides for a safe operating speed, which, to avoid hazardous situations, should not be much less than the speeds on the approaches.





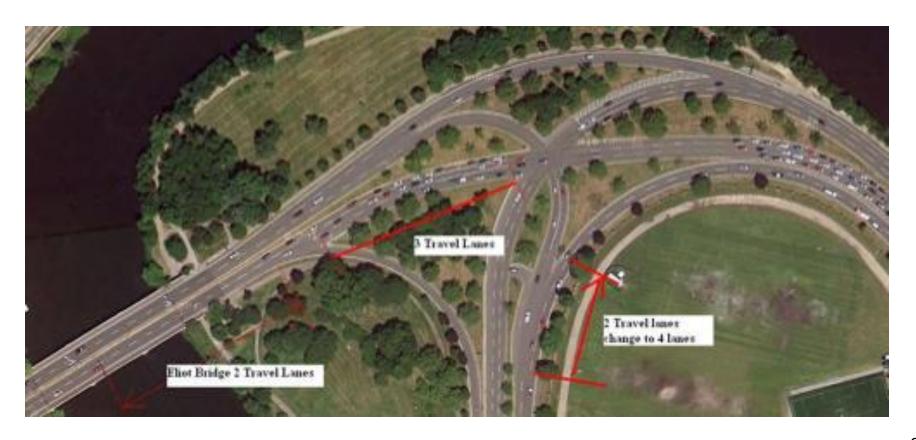
(1) Alignment of At-Grade Intersections

- ■The methods illustrated in Figures (c) and (d) involve the creation of a staggered intersection, In that a single curve is placed at each crossroad leg.
- ■This requires a vehicle on the minor road crossing the intersection to turn first onto the major highway and then back onto the minor highway.
- The realignment illustrated in Figure (d) is preferable because the minor-road vehicle crossing the intersection is required to make a right turn rather than a left turn from the major road to reenter the minor road.
- ■The method illustrated in Figure (c) should be used only when traffic on the minor road is light and when most of this traffic is turning onto and continuing on the major road rather than crossing the intersection.



(1) Alignment of At-Grade Intersections

 Efforts should be made to avoid creating short-radii horizontal curves, since such curves result in the encroachment of drivers on sections of the opposite lanes.



(2) Profile of At-Grade Intersections

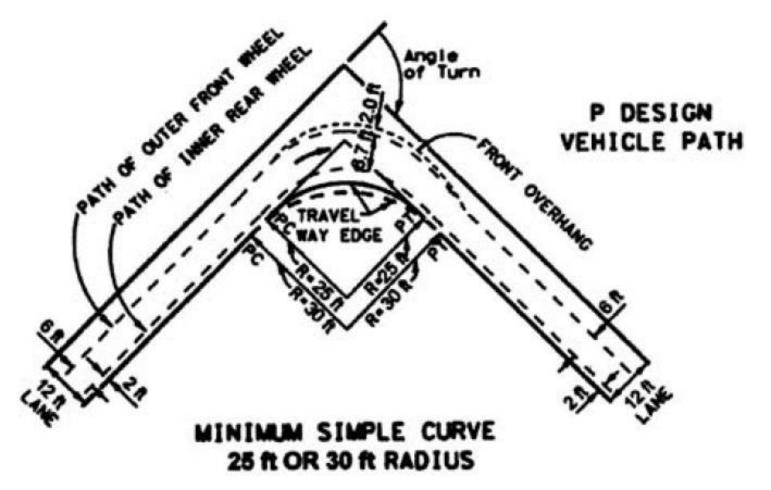
- Wherever possible, large changes in grade should be avoided; preferably, grades should not be > 3 %.
- Significant differences start to occur in stopping and accelerating distances for passenger cars at grades > 3%.

In any case, it is not advisable to use grades higher than 6 percent at intersections.

- When it is necessary to adjust the grade lines of the approaches at an intersection, it is preferable that the grade line of the major highway be continued across the intersection and that of the minor road be altered to obtain the desired result.
- Combination of alignment and grades at an intersection should allow motorists to easily understand the path they should take for any desired direction.

- Main influencing factors:
 - Angle of turn
 - Turning speed
 - Design vehicle
 - Traffic volume
- If turning speed is assumed < 15 mi/h
 - the curves for the pavement edges are designed to conform to at least the minimum turning path of the design vehicle.
- If turning speed is assumed > 15 mi/h
 - minimum turning radius using the design speed should be considered

- If turning speed is assumed < 15 mi/h, three types of design commonly used
 - 1. Simple curve (an arc of a circular curve)



 If turning speed is assumed < 15 mi/h, three types of design commonly used

2. Simple curve with taper VEHICLE PATH TAPER 20 ft RADIUS, OFFSET 2.5 ft

- If turning speed is assumed < 15 mi/h, three types of design commonly used
 - 3. 3-centered compound curve (three simple curves joined together and turning in the same direction)

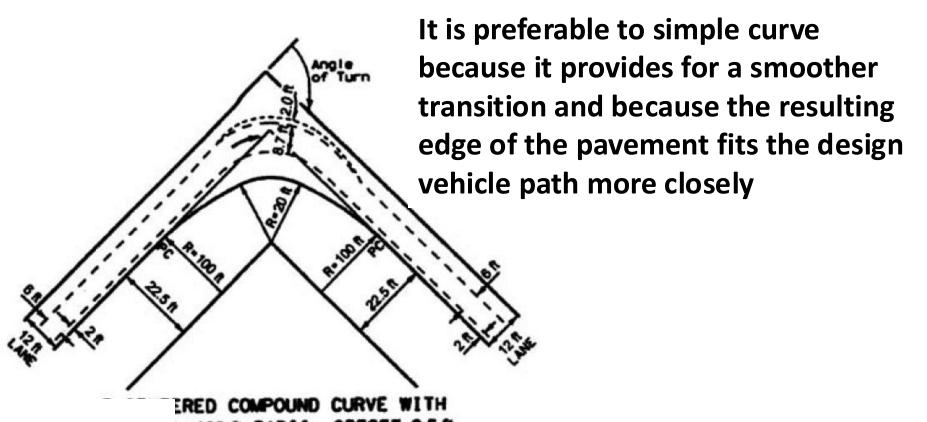


Table 7.2 Minimum Edge of Pavement Design for Turns at Intersections: Simple Curves and Simple Curves with Taper

| Angle of Turn (degree) | Design Vehicle | Simple Curve Radius (ft) | Simple Curve Radius with Taper | | |
|------------------------------|-------------------|-----------------------------|--------------------------------|----------------|--------------|
| | | | Radius (ft) | Offset (ft) | Taper L:T |
| 30 | P | 60 | _ | _ | _ |
| | SU | 100 | _ | _ | _ |
| | WB-40 | 150 | _ | _ | _ |
| | WB-50 | 200 | _ | _ | _ |
| | WB-62 | 360 | 220 | 3.0 | 15:1 |
| | WB-67 | 380 | 220 | 3.0 | 15:1 |
| | WB-100T | 260 | 125 | 3.0 | 15:1 |
| | WB-109D | 475 | 260 | 3.5 | 20:1 |
| 45 | P | 50 | _ | _ | _ |
| | SU | 75 | _ | _ | _ |
| | WB-40 | 120 | _ | _ | _ |
| | WB-50 | 175 | 120 | 2.0 | 15:1 |
| | WB-62 | 230 | 145 | 4.0 | 15:1 |
| | WB-67 | 250 | 145 | 4.5 | 15:1 |
| | WB-100T | 200 | 115 | 2.5 | 15:1 |
| | WB-109D | _ | 200 | 4.5 | 20:1 |
| 60 | P | 40 | _ | _ | _ |
| | SU | 60 | _ | _ | _ |
| | WB-40 | 90 | _ | _ | _ |
| | WB-50 | 150 | 120 | 3.0 | 15:1 |
| | WB-62 | 170 | 140 | 4.0 | 15:1 |
| | WB-67 | 200 | 140 | 4.5 | 15:1 |
| | WB-100T | 150 | 95 | 2.5 | 15:1 |
| | WB-109D | _ | 180 | 4.5 | 20:1 |

Table 7.3 Minimum Edge of Pavement Design for Turns at Intersections: Three-Centered Curves

| | 3-Centered (| 3-Centered Compound | | 3-Centered Compound | |
|-------------------|--|--|--|---|--|
| Design Vehicle | Curve Radii (ft) | Symmetric Offset (ft) | Curve Radii (ft) | Asymmetric Offset (ft) | |
| P | _ | _ | _ | _ | |
| SU | _ | _ | _ | _ | |
| WB-40 | _ | _ | _ | _ | |
| WB-50 | _ | _ | _ | _ | |
| WB-62 | _ | _ | _ | _ | |
| WB-67 | 460-175-460 | 4.0 | 300-175-550 | 2.0-4.5 | |
| WB-100T | 220 -80-220 | 4.5 | 200-80-300 | 2.5-5.0 | |
| WB-109D | 550-250-550 | 5.0 | 250-200-650 | 1.5-7.0 | |
| P | _ | _ | _ | - c | |
| SU | _ | _ | _ | _ | |
| WB-40 | _ | _ | _ | - - | |
| WB-50 | 200-100-200 | 3.0 | _ | _ (C | |
| WB-62 | 460-240-460 | 2.0 | 120-140-500 | 3.0-8.5 | |
| WB-67 | 460-175-460 | 4.0 | 250-125-600 | 1.0-6.0 | |
| WB-100T | 250-80-250 | 4.5 | 200-80-300 | 2.5-5.5 | |
| WB-109D | 550-200-550 | 5.0 | 200-170-650 | 1.5-7.0 | |
| P | _ | _ | _ | _ | |
| SU | _ | _ | _ | _ | |
| WB-40 | _ | _ | _ | _ | |
| WB-50 | 200- 75-200 | 5.5 | 200- 75-275 | 2.0-7.0 | |
| WB-62 | 400-100-400 | 15.0 | 110-100-220 | 10.0-12.5 | |
| WB-67 | 400-100-400 | 8.0 | 250-125-600 | 1.0-6.0 | |
| WB-100T | 250-80-250 | 4.5 | 200-80-300 | 2.0-5.5 | |
| WB-109D | 650-150-650 | 5.5 | 200-140-600 | 1.5-8.0 | |
| | P SU WB-40 WB-50 WB-62 WB-67 WB-100T WB-109D P SU WB-40 WB-50 WB-62 WB-67 WB-100T WB-109D P SU WB-62 WB-67 WB-100T WB-109D | Design Vehicle Curve Radii (ft) P — SU — WB-40 — WB-50 — WB-62 — WB-100T 220 -80-220 WB-109D 550-250-550 P — SU — WB-40 — WB-50 200-100-200 WB-62 460-240-460 WB-67 460-175-460 WB-100T 250- 80-250 WB-109D 550-200-550 P — SU — WB-40 — WB-50 200- 75-200 WB-62 400-100-400 WB-67 400-100-400 WB-67 400-100-400 WB-67 400-100-400 WB-100T 250- 80-250 | Design Vehicle Radii (ft) Symmetric Offset (ft) P — — SU — — WB-40 — — WB-50 — — WB-62 — — WB-67 460-175-460 4.0 WB-100T 220 -80-220 4.5 WB-109D 550-250-550 5.0 P — — SU — — WB-40 — — WB-50 200-100-200 3.0 WB-62 460-240-460 2.0 WB-63 460-175-460 4.0 WB-100T 250- 80-250 4.5 WB-109D 550-200-550 5.0 P — — SU — — WB-40 — — WB-40 — — WB-40 — — WB-50 200- 75-200 5.5 WB-62 400-100-400 <t< td=""><td>Design Vehicle Radii (ft) Symmetric Offset (ft) Curve Radii (ft) P — — — SU — — — WB-40 — — — WB-50 — — — WB-62 — — — WB-100T 220 -80-220 4.5 200- 80-300 WB-109D 550-250-550 5.0 250-200-650 P — — — SU — — — WB-400 — — — WB-50 200-100-200 3.0 — WB-50 200-100-200 3.0 — WB-62 460-240-460 2.0 120-140-500 WB-67 460-175-460 4.0 250-125-600 WB-100T 250- 80-250 4.5 200- 80-300 WB-109D 550-200-550 5.0 200-170-650 P — — — WB-40 — <td< td=""></td<></td></t<> | Design Vehicle Radii (ft) Symmetric Offset (ft) Curve Radii (ft) P — — — SU — — — WB-40 — — — WB-50 — — — WB-62 — — — WB-100T 220 -80-220 4.5 200- 80-300 WB-109D 550-250-550 5.0 250-200-650 P — — — SU — — — WB-400 — — — WB-50 200-100-200 3.0 — WB-50 200-100-200 3.0 — WB-62 460-240-460 2.0 120-140-500 WB-67 460-175-460 4.0 250-125-600 WB-100T 250- 80-250 4.5 200- 80-300 WB-109D 550-200-550 5.0 200-170-650 P — — — WB-40 — <td< td=""></td<> | |

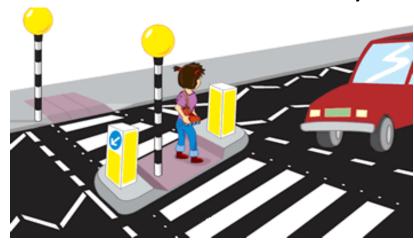
The simple curve with taper closely approximates the 3-centered curve in the field.

- The minimum design for passenger cars is used only
 - at locations where the absolute minimum turns will occur, such as the intersections of local roads with major highways where only occasional turns are made
 - at intersections of two minor highways carrying low volumes
- It is recommended when conditions permit that the minimum design for the SU truck be used.

 Channelization: the separation of conflicting traffic movements into definite paths of travel by traffic islands or pavement markings to facilitate the safe and orderly movements of both vehicles and pedestrians

 Traffic island: the area between traffic lanes that is used to regulate the movement of vehicles or to serve as a pedestrian refuge (Vehicular traffic is excluded

from the island area)



- A properly channelized intersection will result in
 - Increased capacity
 - Enhanced safety
 - Increased driver confidence
- Over-channelization should be avoided since this frequently creates confusion for the motorist and may even result in a lower operating level

Channelization objectives:

- 1. Direct the paths of vehicles so that not more than two paths cross at any one point
- 2. Control the merging, diverging, or crossing angle of vehicles
- Decrease vehicle wander and the area of conflict among vehicles by reducing the amount of paved area
- 4. Provide a clear indication of the proper path for different movements
- 5. Give priority to the predominant movements
- Provide pedestrian refuge
- 7. Provide separate storage lanes for turning vehicles, thereby creating space away from the path of through vehicles for turning vehicles to wait

Channelization objectives:

- Provide space for traffic control devices so that they can be readily seen
- Control prohibited turns
- 10. Separate different traffic movements at signalized intersections with multiple-phase signals
- 11. Restrict the speeds of vehicles

 Based on their physical characteristics, they are classified into:

1. Curbed Traffic Islands: classified into mountable or barrier

- Used mainly in urban highways where approach speed is not excessively high and pedestrian volume is relatively high
- Because of glare, curbed islands may be difficult to see at night

2. Traffic Islands Formed by Pavement Markings

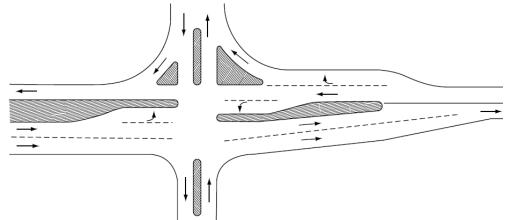
- Flushed island
- Markers include paint, thermoplastic striping, and raised retroreflective markers
- Preferred over curbed islands at intersections where approach speeds are relatively high, pedestrian traffic is low, and signals or sign mountings are not located on the island

3. Islands Formed by Pavement Edges

- Usually unpaved and are mainly used at rural intersections where there is space for large intersection curves
- Based on their function, they are classified into:

1. Channelized islands

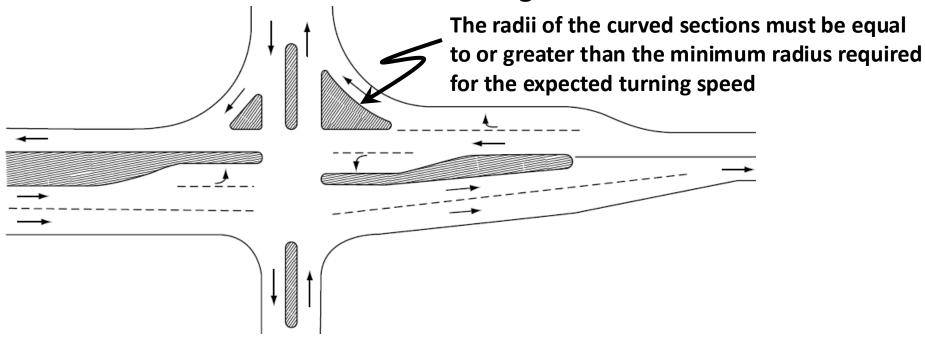
 They eliminate confusion to motorists at intersections with different traffic movements by guiding them into the correct lane for their intended movement





1. Channelized islands

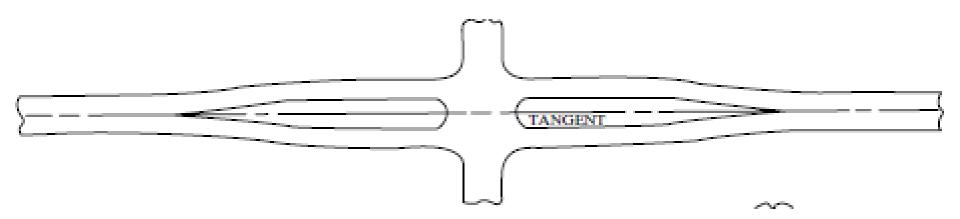
 The outlines of a channelized island should be nearly parallel to the lines of traffic it is channeling

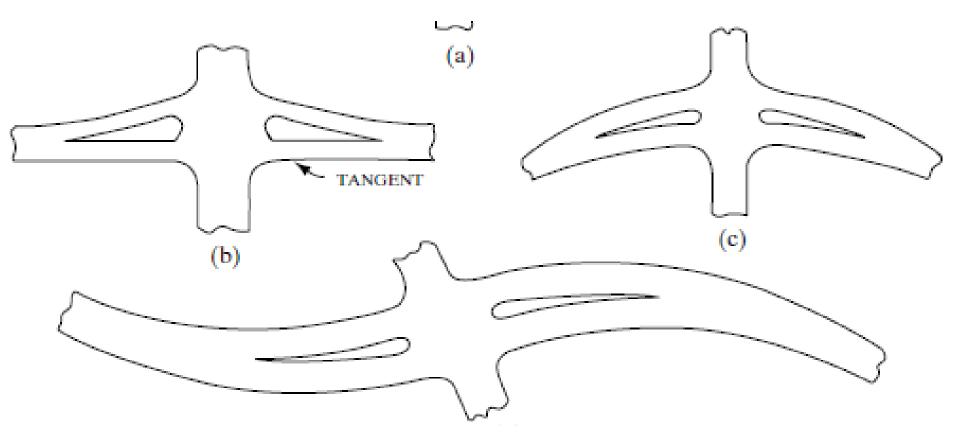


 Number of channelized islands at an intersection should be kept to a practical minimum, since the presence of several islands may cause confusion to the motorist

2. Divisional islands

- They are used to alert drivers that they are approaching an intersection and to control traffic at the intersection
- They also can be used effectively to control left turns at skewed intersections
- The alignment should be designed so that the driver can traverse the intersection easily without any excessive steering





It is sometimes necessary to use reverse curves (two simple curves with opposite curvatures, forming a compound curve) when divisional islands are introduced (particularly when the location is at a tangent)

3. Refuge islands: (pedestrian islands)

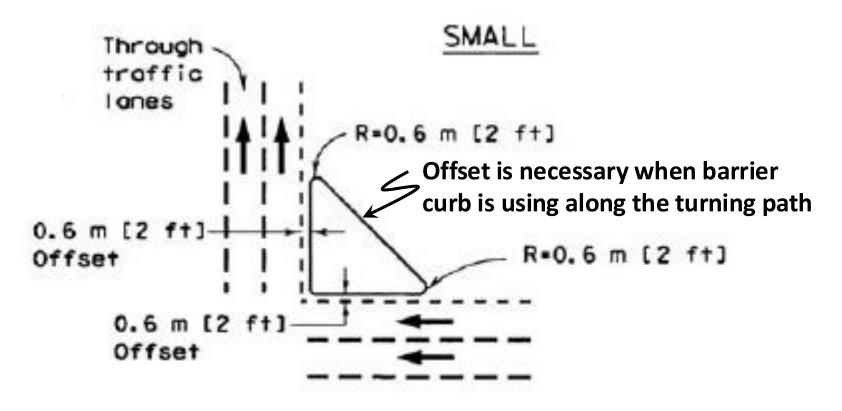
- They are used mainly at urban intersections to serve as refuge areas for wheelchairs and pedestrians crossing wide intersections.
- They also may be used for loading and unloading transit passengers



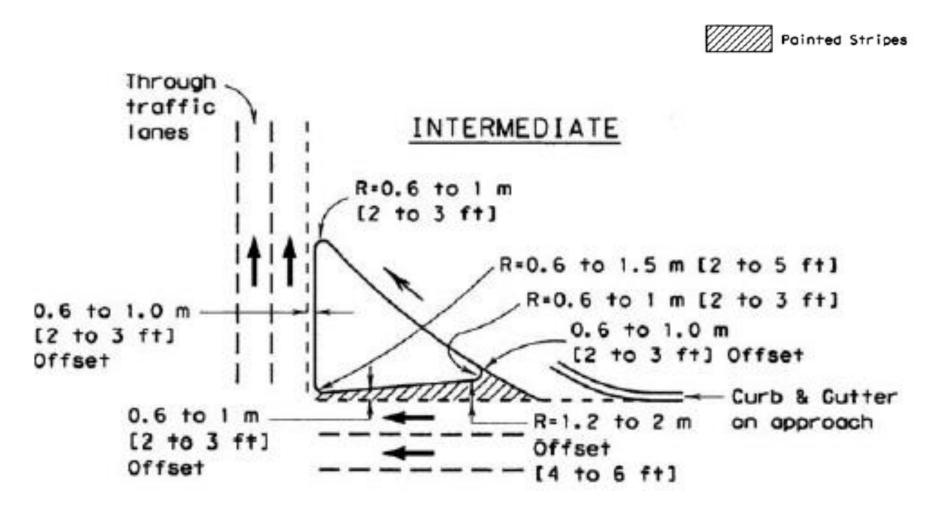
Minimum Sizes of Islands:

- AASHTO recommends that curbed islands have a minimum area of approximately 4.5 m² for urban intersections and 7 m² for rural intersections, although 9 m² ft is preferable for both
- It is not advisable to introduce curbed divisional islands at isolated intersections on high-speed roads,
 - since this may create a hazardous situation unless the island is made visible enough to attract the attention of the driver
- In cases where signs are located on the island, the width of the sign must be considered to ensure that the sign does not extend beyond the limits of the island

- Location and Treatment of Approach Ends of Curbed Islands:
 - The location of a curbed island at an intersection is dictated by the edge of the through traffic lanes and the turning roadways

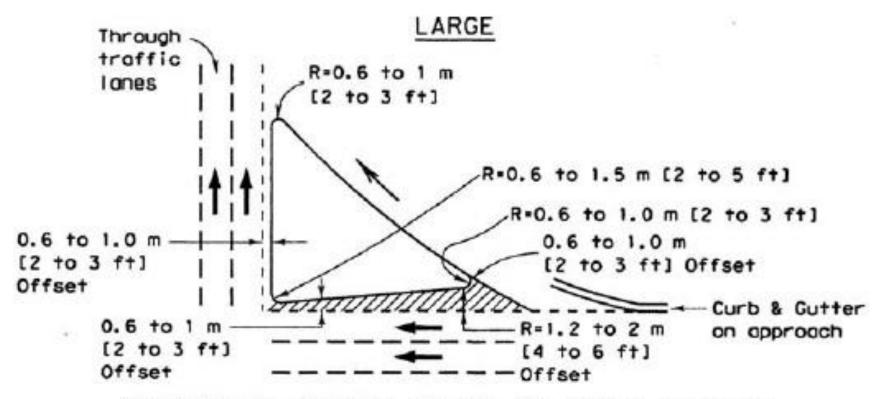


 Location and Treatment of Approach Ends of Curbed Islands:



 Location and Treatment of Approach Ends of Curbed Islands:

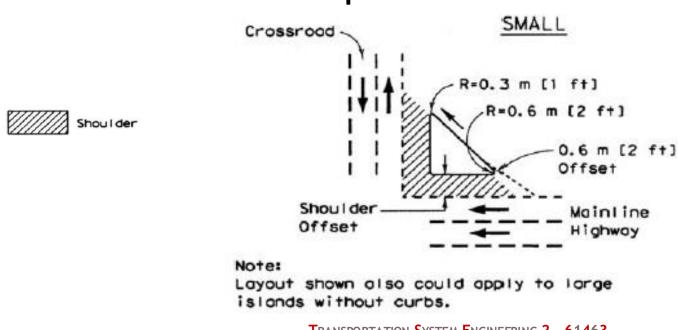
Painted Stripes



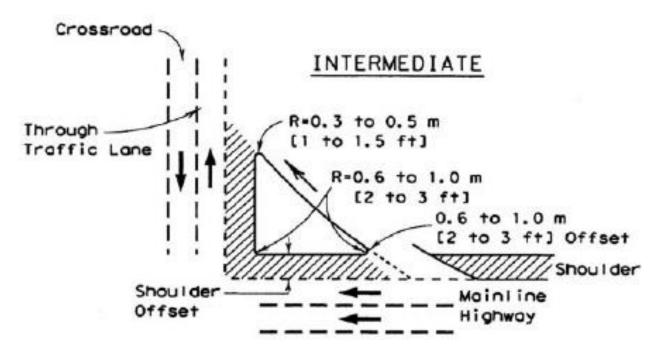
TRIANGULAR CURBED ISLAND ON URBAN STREETS

- Location and Treatment of Approach Ends of Curbed Islands:
 - At intersections with approach shoulders but without deceleration or turn lanes,

The offset of curbed islands from the through travel lane should be equal to the width of the shoulder

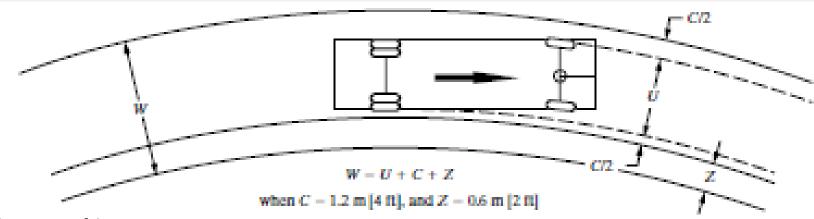


- Location and Treatment of Approach Ends of Curbed Islands:
 - If deceleration lane precedes the curbed island, or when a gradually widened auxiliary pavement exists and speeds are within the intermediate-to-high range,
 - it is desirable to increase the offset of the nose by an additional 0.6 to 1.2 m



- In cases where vehicle speeds are expected to be greater than 15 mi/h, it is necessary to increase the pavement widths of the turning roadways
- Three classifications of pavement widths:
 - Case I: one-lane, one-way operation with no provision for passing a stalled vehicle
 - Case II: one-lane, one-way operation with provision for passing a stalled vehicle
 - Case III: two-lane operation, either one-way or two-way

- The pavement width for each case depends on:
 - Radius of the turning roadway
 - Characteristics of the design vehicle
- The pavement width depends on:
 - Widths of the front and rear overhangs $\mathbf{F}_{\!A}$ and $\mathbf{F}_{\!B}$ of the design vehicle,
 - Total clearance per vehicle C,
 - An extra width allowance due to difficulty of driving on curves **Z**,
 - Track width **U** of the vehicle as it moves around the curve.

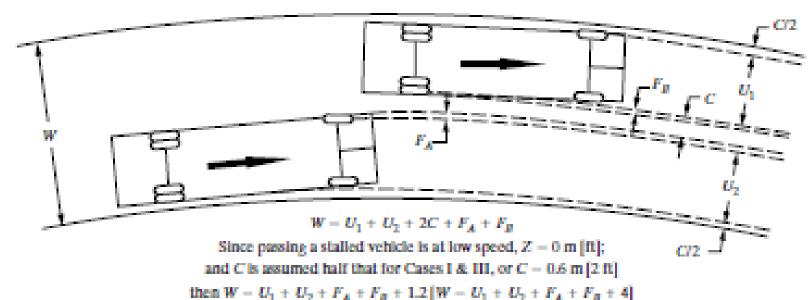


F_A can be ignored in Case I, as no passing maneuver is involved

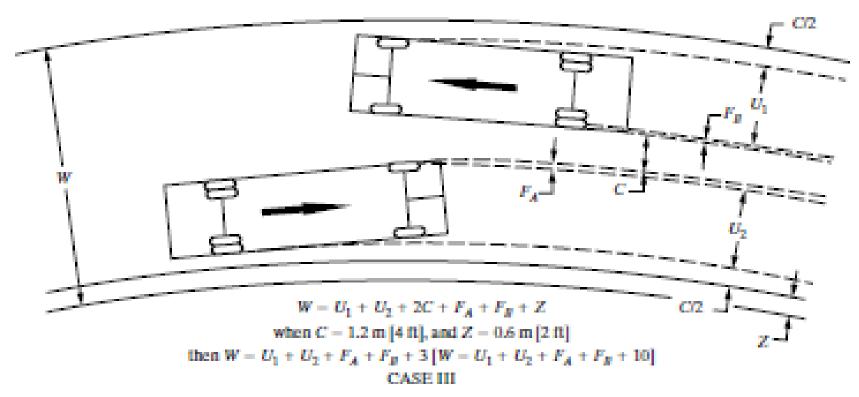
then W = U + 1.8 [W - U + 6]

CASE I

One-Lane One-Way Operation-No Passing



CASE II
One—Lane One—Way Operation Provision for Passing Stalled Vehicle



Two-Lane Operation-One or Two Way

U – Track width of vehicle (out–to–out tires), m [ft]

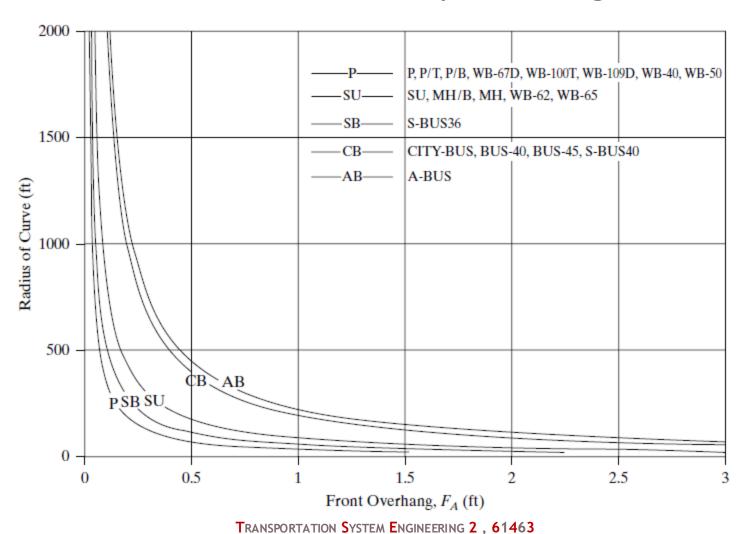
F_A — Width of front overhang, m [ft]

 F_B — Width of rear overhang, m [ft]

C — Total lateral clearance per vehicle, m [ft]

 Z – Extra width allowance due to difficulty of driving on curves, m [ft]

• Values for the front overhang F_A for different vehicle types can be obtained directly from Figure 7.18



- The width of the rear overhang F_B is usually taken as
 - 0.15 m (0.5 ft) for passenger cars
 - 0 m for truck vehicles
- The lateral clearance **C** can be taken as:
 - 4 ft for Case I
 - 2 ft for the stopped vehicle and 2 ft for the passing vehicle in
 Case II
 - 4 ft for Case III
- The extra width allowance Z is estimated as:

Z = extra width allowance to compensate for the difficulty in maneuvering (ft)

v = design speed (mi/h)

R = radius of curve (ft)

$$Z = \frac{v}{\sqrt{R}}$$

 The track width U for passenger cars and single-unit trucks is given as:

$$U = u + R - \sqrt{(R^2 - \sum L_i^2)}$$

U = track width on curve (ft)

u = track width on tangent (out-to-out of tires) (ft)

R = radius of curve or turn (ft)

 L_i = wheelbase of design vehicle between consecutive axles or (sets of tandem axles) and articulation points (ft)

- Pavement widths are seldom designed for a single vehicle type, since the highway should be capable of accommodating different types of vehicles, especially when provision is made for passing
- Design of the pavement width is therefore based on three types of traffic conditions
 - Traffic Condition A: Passenger vehicles are predominant, but this traffic condition also provides some consideration for the occasional SU truck
 - Traffic Condition B: Proportion of SU vehicles warrants this vehicle type to be the design vehicle but it allows for the accommodation of some tractor-trailer combination trucks (5 to 10%)
 - Traffic Condition C: Design vehicle is WB-12 or WB-15 (WB-40 or WB-50)

Minimum pavement width for turning roadways

Table 7.5 Design Widths of Pavements for Turning Roadways

| Table 7.5 Desi | gn wiatn | S OF Paverr | ients for t | urning Roa | iuways | | | | |
|---|--|--|--------------|---|--|------------------------|---|------------------|----|
| | | | U.S | s. CUSTO | MARY | | | | |
| Radius on inner edge of | Provi | Case I Lane, One peration—i sion for Pa talled Veh | No assing | Op Provi a S | Case II Lane, One eration—v sion for Po talled Veh | vith assing icle | Case III Two-Lane Operation— Either One-Way or Two-Way | | |
| pavement | | | | Design | Traffic Co | nditions | | | |
| R(ft) | A | B | C | A | B | C | A | \boldsymbol{B} | C |
| 50 | 18 | 18 | 23 | 20 | 26 | 30 | 31 | 36 | 45 |
| 75 | 16 | 17 | 20 | 19 | 23 | 27 | 29 | 33 | 38 |
| 100 | 15 | 16 | 18 | 18 | 22 | 25 | 28 | 31 | 35 |
| 150 | 14 | 15 | 17 | 18 | 21 | 23 | 26 | 29 | 32 |
| 200 | 13 | 15 | 16 | 17 | 20 | 22 | 26 | 28 | 30 |
| 300 | 13 | 15 | 15 | 17 | 20 | 22 | 25 | 28 | 29 |
| 400 | 13 | 15 | 15 | 17 | 19 | 21 | 25 | 27 | 28 |
| 500 | 12 | 15 | 15 | 17 | 19 | 21 | 25 | 27 | 28 |
| Tangent | 12 | 14 | 14 | 17 | 18 | 20 | 24 | 26 | 26 |
| | | | Width . | Modification | on Regard | ing Edge T | reatment | | |
| No stabilized shoulder | | None | | | None | | | None | |
| Sloping curb | | None | | None | | | None | | |
| Vertical curb: One side Two sides | Add 1 ft Add 2 ft | | | None Add 1 ft | | | Add 1 ft Add 2 ft | | |
| Stabilized shoulder, one or both sides | Lane width for conditions B&C on tangent may be reduced to 12 ft where shoulder is 4 ft or wider | | | Deduct shoulder width; minimum pavement width as under Case I | | | Deduct 2 ft where shoulder is 4 ft or wider | | |

Design Vehicles in Combination

Table 7.6 Design Vehicles in Combination

(a) Design Vehicles in Combination that Provide the Full Clear Width (C)

| Design Traffic Condition | |
|--------------------------|-------|
| В | C |
| SII | WR.40 |

| Case | A | B | C |
|------|------|-------|-------------|
| I | P | SU | WB-40 |
| П | P-P | P-SU | SU-SU |
| III | P-SU | SU-SU | WB-40-WB-40 |

(b) Larger Vehicles that Can Be Operated

| | | - 5 | | | ATT 1 | The same of the sa |
|-----|-------|-----|--------|-----|------------|--|
| | esign | - 1 | 200000 | 100 | Company of | ALC: NAME OF STREET |
| 4.0 | | - 4 | 0.000 | | V-10/2004 | 4445-770 |
| | | | | | | |

 $D_{i_1, \dots, i_m} = T_{i_1, \dots, i_m} C_{i_1, \dots, i_m} J_{i_2, \dots, i_m}$

| Case | A | В | С |
|------|----------|-------------|-------------|
| I | WB-40 | WB-40 | WB-50 |
| II | P-SU | P-WB-40 | SU-WB-40 |
| III | SU-WB-40 | WB-40-WB-40 | WB-50-WB-50 |

SOURCE: A Policy on Geometric Design of Highways and Streets, The American Association of State Highway and Transportation Officials, Washington, D.C., 2004. Used with permission.

This will result in reduced clearance between vehicles that will vary from about one-half the value of *C for sharper* curves to nearly the full value of C for flatter curves.

Example 7.1

Example 7.1 Determining the Width of a Turning Roadway at an Intersection

A ramp from an urban expressway with a design speed of 30 mi/h connects with a local road forming a T intersection. An additional lane is provided on the local road to allow vehicles on the ramp to turn right onto the local road without stopping. The turning roadway has a mountable curb on one side and will provide for a one-lane, one-way operation with provision for passing a stalled vehicle. Determine the width of the turning roadway if the predominant vehicles on the ramp are single-unit trucks but give some consideration to semitrailer vehicles. Use 0.08 for the superelevation.

Solution:

Determine the minimum radius of the curve.
 Because the speed is greater than 15 mi/h, use Eq. 3.33 of Chapter 3 and a value of 0.20 for f_s (from Table 3.3):

$$R = \frac{u^2}{15(e + f_s)}$$
$$= \frac{30^2}{15(0.08 + 0.2)}$$
$$= 214.29 \text{ ft}$$

Use 215 ft.

Determine the type of operation and traffic condition.

The operational requirements, one-lane, one-way with provision for passing a stalled vehicle require Case II operation.

The traffic condition, single-unit trucks but with some consideration given to semitrailer vehicles, requires Traffic Condition B.

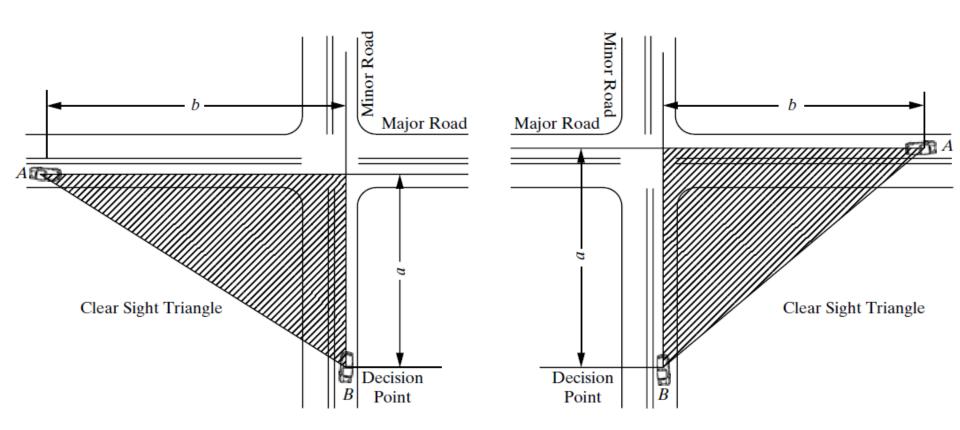
Determine the turning roadway width.
 Use Table 7.5, with R = 212 ft, Traffic Condition B, and Case II.

Pavement width = 20 ft

Since the turning roadway has a mountable curb only on one side, no modification to the width is required.

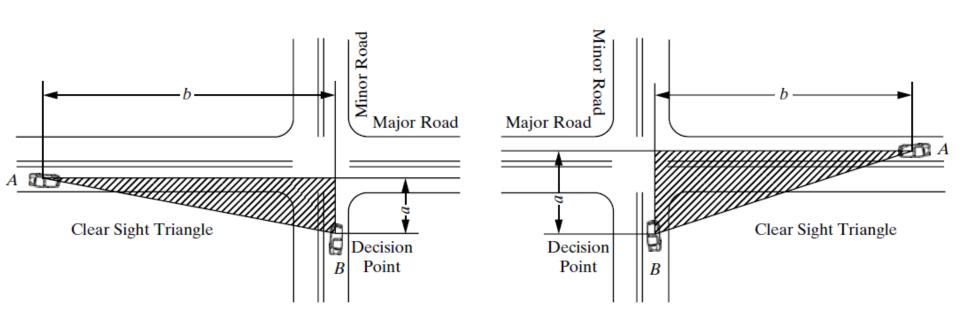
- High crash potential can be reduced by providing sight distances that allow drivers to have an unobstructed view of the entire intersection at a distance great enough to permit control of the vehicle
- Two types of sight triangles:
 - 1. Approach sight triangles: It allows for the drivers on both the major roads and minor roads to see approaching intersecting vehicles in sufficient time to avoid a potential collision by reducing the vehicle's speed or by stopping.
 - 2. Departure sight triangles: It allows for the driver of a stopped vehicle on the minor road to enter or cross the major road without conflicting with an approaching vehicle from either direction of the major road

Approach sight triangles



(a) Approach Sight Triangles (uncontrolled or yield-control)

Departure sight triangles



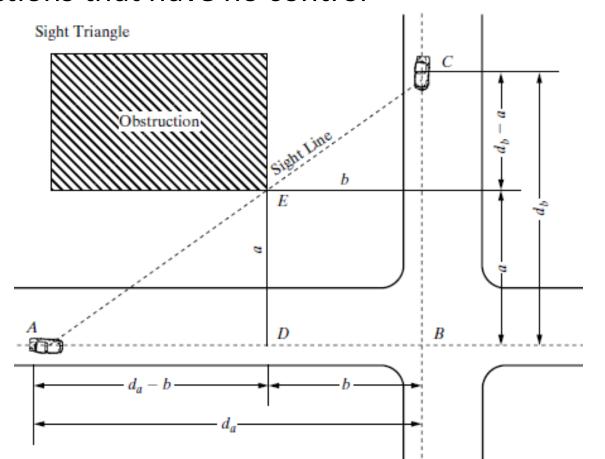
(b) Departure Sight Triangles (stop control)

- A sight obstruction is considered as an object having a minimum height of 4.35 ft (1.33 m) that can be seen by a driver with an eye height of:
 - 3.5 ft (1.00 m) for a passenger car
 - 7.6 ft (2.3 m) for truck
- The lengths of the legs of the sight triangle depends on:
 - Major road speed
 - Minor road speed
 - Type of control

- There are four cases for at-grade intersections:
 - Case A: With no control
 - Case B: With stop control on the minor road
 - Case C: With yield control on the minor road
 - Case D: With traffic signal control

Case A: With no control

 AASHTO has noted that drivers tend to decrease their speeds to about 50% of their mid-block speed as they approach intersections that have no control



- Case A: With no control
 - From triangle similarity:

From Table 7.7
$$\frac{d_b}{d_a} = \frac{a}{d_a - b}$$

Case A: With no control

Table 7.7 Suggested Lengths and Adjustments of Sight-Triangle Leg Case A—No Traffic Control

| Design Speed (mi/h) | Length of Leg (ft) |
|---------------------|--------------------|
| 15 | 70 |
| 20 | 90 |
| 25 | 115 |
| 30 | 140 |
| 35 | 165 |
| 40 | 195 |
| 45 | 220 |
| 50 | 245 |
| 55 | 285 |
| 60 | 325 |
| 65 | 365 |
| 70 | 405 |
| 75 | 445 |
| 80 | 485 |

(a)

it should be noted that these distances tend to be lower than stopping sight distance because drivers tend to reduce their speeds as they approach intersections with no controls

Case A: With no control

Table 7.7 Suggested Lengths and Adjustments of Sight-Triangle Leg Case A—No Traffic Control

| Approac Grade | h | | | | | Desi | gn Spe | ed (m | i/h) | | | | | |
|------------------|-----|-----|-----|-----|-----|------|--------|-------|------|-----|-----|-----|-----|-----|
| (%) | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 80 |
| -6 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 |
| -5 | 1.0 | 1.0 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.2 | 1.2 | 1.2 | 1.2 |
| -4 | 1.0 | 1.0 | 1.0 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| -3 to 3 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| +4 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 |
| +5 | 1.0 | 1.0 | 1.0 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 |
| +6 | 1.0 | 1.0 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 |

(b)

Example 7.2

Example 7.2 Computing Speed Limit on a Local Road

A tall building is located 45 ft from the centerline of the right lane of a local road (b in Figure 7.20) and 65 ft from the centerline of the right lane of an intersecting road (a in Figure 7.20). If the maximum speed limit on the intersecting road is 35 mi/h, what should the speed limit on the local road be such that the minimum sight distance is provided to allow the drivers of approaching vehicles to avoid imminent collision by adjusting their speeds? Approach grades are 2%.

Solution:

 Determine the distance on the local road at which the driver first sees traffic on the intersecting road.

Speed limit on intersecting road = 35 mi/h

Distance required on intersecting road (d_a) = 165 ft (from Table 7.7)

Calculate the distance available on local road by using Eq. 7.4

$$d_b = a \frac{d_a}{d_a - b}$$
= $65 \frac{165}{165 - 45}$
= 89.37 ft

• Determine the maximum speed allowable on the local road.

The maximum speed allowable on local road is 20 mi/h (from Table 7.7). No correction is required for the approach grade as it is less than 3%.

- Case C: With yield control on the minor road
 - Sight Distance Requirement for Crossing a Yield Controlled
 Intersection from a Minor Road
 - Assumption made is similar to that used for the no-control maneuver in Case A, but with the following modifications:
 - Drivers on minor roads tend to decelerate to 60 percent of the minor road design
 - The rate of deceleration is 5 ft /sec² (1.5 m/sec²)
 - The time t_g to cross the intersection should include the time taken for the vehicle to travel from the decision point where the deceleration begins to where the speed is reduced to 60 percent of the minor road design speed
 - The vehicle then travels at the reduced speed until it crosses and clears the intersection

- Case C: With yield control on the minor road
 - The length of the sight distance (d_{ISD}) :

$$t_g = t_a + (w + L_a)/0.88v_{\text{minor}}$$
$$d_{\text{ISD}} = 1.47v_{\text{major}}t_g$$

 t_g = travel time to reach and clear the intersection (sec)

 t_a = travel time to reach the major road from the decision point for a vehicle that does not stop

w =width of the intersection to be crossed (ft)

 L_a = length of design vehicle (ft)

 $v_{\text{minor}} = \text{design speed of minor road (mi/h)}$

 $v_{\text{major}} = \text{design speed of major road (mi/h)}$

• Case C: With yield control on the minor road

$$(t_g) = (t_a) + (w + L_a)/0.88v_{\text{minor}}$$
 $d_{\text{ISD}} = 1.47v_{\text{major}}t_g$

Table 7.9 Case C1—Crossing Maneuvers from Yield-Controlled Approaches—Length of Minor Road Leg and Travel Times

| | Minor-Road | Approach | Travel Time t_g (seconds) | | | |
|------------------------|------------------------------------|-----------------------------------|-----------------------------|--------------------------------|--|--|
| Design Speed (mi/h) | Length of Leg ¹ (ft) | Travel Time $t_a^{1,2}$ (seconds) | Calculated Value | Design Value ^{3,4} | | |
| 15 | 75 | 3.4 | 6.7 | 6.7 | | |
| 20 | 100 | 3.7 | 6.1 | 6.5 | | |
| 25 | 130 | 4.0 | 6.0 | 6.5 | | |
| 30 | 160 | 4.3 | 5.9 | 6.5 | | |
| 35 | 195 | 4.6 | 6.0 | 6.5 | | |
| 40 | 235 | 4.9 | 6.1 | 6.5 | | |
| 45 | 275 | 5.2 | 6.3 | 6.5 | | |
| 50 | 320 | 5.5 | 6.5 | 6.5 | | |
| 55 | 370 | 5.8 | 6.7 | 6.7 | | |
| 60 | 420 | 6.1 | 6.9 | 6.9 | | |
| 65 | 470 | 6.4 | 7.2 | 7.2 | | |
| 70 | 530 | 6.7 | 7.4 | 7.4 | | |
| 75 | 590 | 7.0 | 7.7 | 7.7 | | |
| 80 | 660 | 7.3 | 7.9 | 7.9 | | |

- Case C: With yield control on the minor road
 - Length of the sight distance (d_{ISD}) is estimated in Table 7.10

Table 7.10 Length of Sight Triangle Leg along Major Road—Case C1—Crossing Maneuver at Yield-Controlled Intersection

| Major Road Design Speed | Stopping Sight Distance | | | M | Ainor-Rod | ıd Design | Speed (n | ni/h) | |
|----------------------------------|-------------------------------|-----|-------|-----|-----------|-----------|----------|-------|-----|
| (mi/h) | (ft) | 15 | 20-50 | 55 | 60 | 65 | 70 | 75 | 80 |
| 15 | 80 | 150 | 145 | 150 | 155 | 160 | 165 | 170 | 175 |
| 20 | 115 | 200 | 195 | 200 | 205 | 215 | 220 | 230 | 235 |
| 25 | 155 | 250 | 240 | 250 | 255 | 265 | 275 | 285 | 295 |
| 30 | 200 | 300 | 290 | 300 | 305 | 320 | 330 | 340 | 350 |
| 35 | 250 | 345 | 335 | 345 | 360 | 375 | 385 | 400 | 410 |
| 40 | 305 | 395 | 385 | 395 | 410 | 425 | 440 | 455 | 465 |
| 45 | 360 | 445 | 430 | 445 | 460 | 480 | 490 | 510 | 525 |
| 50 | 425 | 495 | 480 | 495 | 510 | 530 | 545 | 570 | 585 |
| 55 | 495 | 545 | 530 | 545 | 560 | 585 | 600 | 625 | 640 |
| 60 | 570 | 595 | 575 | 595 | 610 | 640 | 655 | 680 | 700 |
| 65 | 645 | 645 | 625 | 645 | 660 | 690 | 710 | 740 | 755 |
| 70 | 730 | 690 | 670 | 690 | 715 | 745 | 765 | 795 | 815 |
| 75 | 820 | 740 | 720 | 740 | 765 | 795 | 795 | 850 | 875 |
| 80 | 910 | 790 | 765 | 790 | 815 | 850 | 850 | 910 | 930 |

- Case C: With yield control on the minor road
 - It should be noted that these values are for a passenger car as the design vehicle, and approach grades of 3 percent or less.
 - Appropriate corrections should be made when the grade is higher than 3 percent.

Example 7.5

Example 7.5 Determining the Minimum Sight Distance for Crossing at an Intersection with Yield Control

An urban two-lane minor road crosses a four-lane divided highway with a speed limit of 55 mi/h. If the minor road has a speed limit of 35 mi/h and the intersection is controlled by a yield sign on the minor road, determine the sight distance from the intersection that is required along the major road such that the driver of a vehicle on the minor road can safely cross the intersection. The following conditions exist at the intersection.

Major road lane width = 11 ft

Median width = 8 ft

Design vehicle on minor road is a passenger car length = 22 ft

Approach grade on minor road = 3%.

Solution: Use Eq. 7.6 to determine time (t_a) as the travel time to reach and clear the intersection.

$$t_g = t_a + (w + L_a)/0.88v_{\rm min}$$
 $t_a = 5.2 \, {\rm sec} \, {\rm for} \, {\rm passenger} \, {\rm vehicles} \, {\rm from} \, {\rm Table} \, 7.9$
 ${\bf w} = (4 \times 11 + 8) = 52 \, {\rm ft}$
 $t_g = 5.2 + (52 + 22)/(0.88 \times 35)$
 $= 7.6 \, {\rm sec}$

Use Eq. 7.7 to determine the length of the sight on the major road.

$$d_{\text{ISD}} = 1.47 v_{\text{major}} t_g$$

= 1.47 × 55 × 7.6 = 614.5 ft